



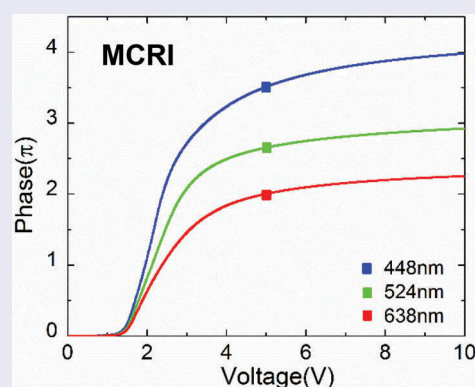
## High-frame-rate liquid crystal phase modulator for augmented reality displays

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### ABSTRACT

We optimise a new liquid crystal mixture with wide nematic range, high birefringence ( $\Delta n$ ), high resistivity, moderate dielectric anisotropy ( $\Delta\epsilon$ ) and relatively low rotational viscosity for augmented reality display applications. High  $\Delta n$  and large  $\Delta\epsilon$  allow a thin cell gap ( $d \approx 1.5 \mu\text{m}$ ) to be employed in a reflective liquid-crystal-on-silicon (LCoS) device to achieve  $2\pi$  phase change at 5 V and 2.87 ms average phase-to-phase response time at 40°C without complicated overdrive circuitry. Such a fast response time enables an LCoS panel to achieve 240 Hz frame rate for field sequential colour operation to avoid image flickering.



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## 1. Introduction

Liquid-crystal-on-silicon (LCoS) panel has been widely used for intensity modulation in augmented reality (AR) displays, such as Google Glass and Microsoft HoloLens, because of its high resolution, low driving voltage and low power consumption [1–3]. To overcome the focus-cue mismatch issue, phase-only LCoS has found useful applications in focal surface displays [4–6]. For these applications, a large phase modulation depth ( $\geq 2\pi$ ) is required. Meanwhile, the liquid crystal (LC) response time should be less than 4 ms in order to achieve the desired 240 Hz frame rate. From [4,5], both Oculus and Microsoft devices were operated at 60 Hz, which is 4 times too slow to meet the required 240 Hz. Therefore, there is urgent need to develop a phase-only LCoS device with response time less than 4 ms,

while keeping a  $2\pi$  phase change and low operation voltage ( $< 6$  V) without the overdrive and undershoot driving circuitry [7].

To improve response time, several approaches have been investigated, such as dual-frequency LCs [8], polymer-stabilised blue-phase LCs [9–11], ferroelectric LCs [12,13] and polymer network LCs [14,15]. Each technology has its own pros and cons, and it is still quite challenging to satisfy all the above-mentioned requirements. For example, the complicated driving scheme of dual-frequency LCs, the high operation voltage of polymer-stabilised LCs and the bistability of ferroelectric LCs remain to be solved for LCoS-based phase modulators. Lately, a low viscosity and negative dielectric anisotropy ( $\Delta\epsilon$ ) LC mixture has been developed to achieve submillisecond response time for VA LCoS intensity modulator by using a thin cell gap

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( $d \approx 1.2 \mu\text{m}$ ) [7]. However, to achieve  $2\pi$  phase change, its response time would increase by 4 times, because the required cell gap is twice thicker than that of the corresponding intensity modulator. Recently, three positive  $\Delta\epsilon$  and low-viscosity LC mixtures with fast response time have been reported for 240 Hz phase-only LCoS devices [16], but their resistivity remains to be improved, which determines the voltage holding ratio in operation. These two reports employed low  $\gamma_1/K_{11}$  LCs to improve the response time for the applications of LCoS devices. Another common way is to use a high  $\Delta n$  LC to reduce cell gap for achieving faster response time. However, the high melting point and large viscosity of high  $\Delta n$  LC mixtures are concerns for LCoS-based phase modulators.

In this article, we reported two high  $\Delta n$  LC mixtures and one commercial high  $\Delta n$  LC mixture to know how material parameters affect the LC response time in LCoS-based phase modulators. Finally, we optimised a new nematic LC mixture, designated as MCRI, for LCoS-based phase modulators to achieve fast response time without the need of overdrive circuitry. MCRI exhibits a high birefringence ( $\Delta n \sim 0.28$  at  $T = 25^\circ\text{C}$  and  $\lambda = 550 \text{ nm}$ ), moderate rotational viscosity and dielectric anisotropy ( $\Delta\epsilon \sim 7.6$ ). By using a thin cell gap ( $d \approx 1.5 \mu\text{m}$ ), we can achieve  $2\pi$  phase change at 5 V and 240 Hz frame rate. Therefore, MCRI is expected to find useful applications for the emerging AR displays.

## 2. Material development

### 2.1 Components

As shown in Table 1, fluorine-containing diphenyl acetylene type LCs (#1-#3) [17], new diluter (#6) [18] and new highly fluorinated LCs (#7, #8) [19,20] were synthesised according to similar literature procedures. Here, R represents different alkyl chain. The tolane LCs (#4, #5) were purchased from Xi'an Caijing Opto-Electrical Science Technology and used as received. The commercial high  $\Delta n$  LC mixture (HTD028200-200) was purchased from Jiangsu Hecheng Advanced Materials and also used as received. The phase transition temperatures were measured by differential scanning calorimetry (DSC, TA instruments Q100) in nitrogen at the heating and cooling rate of  $2^\circ\text{C min}^{-1}$ , and POM, LEICA DM2500P with Linkam THMS600 hot-stage and control unit at a heating and cooling rate of  $0.5^\circ\text{C min}^{-1}$ . The phase transition temperatures reported in this article were the peak values of the transition on DSC curves.

**Table 1.** Chemical structures of our LC mixtures.

No.	Structures	Melting points ( $^\circ\text{C}$ ) <sup>a</sup>	Clearing points ( $^\circ\text{C}$ ) <sup>a</sup>
1		80.0	163.5
2		59.5	118.4
3		55.0	64.4
4		66	-
5		53.1	81.1
6		33.6	39.2
7		54.4	106.0
8		53.8	114.6

<sup>a</sup>The alkyl chain of each compound is *n*-propyl, except that of compound #5 represents *n*-butyl.

### 2.2 LC mixtures formulation

To obtain high resistivity and low viscosity simultaneously, fluorinated tolane is a good candidate. Therefore, a high  $\Delta n$  and high resistivity LC mixture was prepared by our synthetic compounds #1-#5 (SNNU-1): its physical properties are listed as follows:  $\Delta n = 0.337$  at  $\lambda = 550 \text{ nm}$ ,  $\Delta\epsilon = 2.86$ , visco-elastic constant  $\gamma_1/K_{11} = 17.5 \text{ ms}/\mu\text{m}^2$ , high resistivity  $> 10^{13} \Omega \cdot \text{cm}$ , melting temperature  $T_m = -18^\circ\text{C}$  and clearing temperature  $T_c = 123^\circ\text{C}$ . Its birefringence is reasonably high, but its  $\Delta\epsilon$ , rotational viscosity  $\gamma_1$  and melting point still need improvement.

To reduce melting point and  $\gamma_1$ , we added 15.0 wt% of a new diluter (#6) to SNNU-1. Firstly, to maintain high  $\Delta n$  and increase  $\Delta\epsilon$ , we attempted a high  $\Delta n$

(0.21), large  $\Delta\epsilon$  (20.4) and relatively low viscosity (151.7 mPa·s) LC (#7), while it was difficult to blend in the LC mixture. After optimisation, to maintain high resistivity and increase  $\Delta\epsilon$ , we added 20.2 wt% of thin-film-transistor (TFT) LC (#8) with a relatively low  $\Delta n$  (0.14), large  $\Delta\epsilon$  (25.8), relatively large viscosity (360.0 mPa·s) and good solubility to prepare a new LC mixture MCRI (compounds #1-#6, #8).

Meanwhile, we selected a commercial LC mixture (HTD028200-200) for comparison (not listed in Table 1). As a common issue for high  $\Delta n$  and large  $\Delta\epsilon$  LC mixtures, its relatively low resistivity ( $> 2 \times 10^{11}$ ) hinders its application for phase LCoS. Another general concern for high  $\Delta n$  LC materials is their UV stability [21,22]. To prevent photo-degradation, we recommend blocking the LC area from UV exposure during sealing process.

### 3. Material characterisation

Table 2 lists the measured physical properties of the three LC mixtures. The measurement was conducted at 40°C – the actual operating temperature of a working LCoS device, due to the thermal effects of backplane and illumination light [23].

#### 3.1 Birefringence

To measure  $\Delta n$ , each LC mixture was injected into a homogeneous cell with cell gap  $d \approx 5 \mu\text{m}$ . The pretit angle of the rubbed polyimide alignment layers is about 3°. The cell was mounted in a Linkam LTS 350 Large Area Heating/Freezing Stage controlled by TMS94 Temperature Programmer and then sandwiched between two crossed polarisers. A 1 kHz square-wave AC voltage was applied to the LC cell. The birefringence was calculated from the measured phase retardation [24]. Figure 1(a) depicts the temperature-dependent birefringence at  $\lambda = 633 \text{ nm}$  (He-Ne laser). At  $\lambda = 633 \text{ nm}$  and 40°C, the  $\Delta n$  of [SNUU-1, MCRI, HTD028200-200] is [0.2810, 0.2531, 0.2719], respectively (Table 2). The extrapolated birefringence  $\Delta n_0$  at  $T = 0 \text{ K}$  and the exponent  $\beta$  were obtained by fitting

**Table 2.** Measured physical properties of three LC mixtures at  $T = 40^\circ\text{C}$ .

LC mixture	$T_m$ (°C)	$T_c$ (°C)	$\Delta n$ at		$\gamma_1/K_{11}$	$\gamma_1$ (mPa·s)	$K_{11}$ (pN)
			633 nm	$\Delta\epsilon$			
SNUU-1	-18.2	123.3	0.2810	2.59	8.58	120.1	14.0
MCRI	-38.3	107.4	0.2531	6.65	8.70	132.9	15.3
HTD028200-200	-20.1	103.2	0.2719	6.83	11.55	109.7	9.5

the experimental data with Equation (1) [25] and the results are listed in Table S1.

$$\Delta n = \Delta n_0 S = \Delta n_0 (1 - T/T_c)^\beta. \quad (1)$$

Moreover, to investigate the electro-optic performance at different colours, a tunable Argon ion laser ( $\lambda = 457, 488$  and  $514 \text{ nm}$ ) and a He-Ne laser ( $\lambda = 633 \text{ nm}$ ) were used for the characterisation. We fitted the measured wavelength-dependent  $\Delta n$  (dots in Figure 1(b)) with the single-band birefringence dispersion equation [26]:

$$\Delta n = G \frac{\lambda^2 \lambda^{*2}}{\lambda^2 - \lambda^{*2}}, \quad (2)$$

where  $G$  is a proportionality constant and  $\lambda^*$  is the mean resonance wavelength. The obtained  $G$  and  $\lambda^*$  values are listed in Table S1.

#### 3.2 Visco-elastic coefficient

The rotational viscosity  $\gamma_1$  and splay elastic constant [ $K_{11}$ ] were measured through transient current method by autronic-MELCHRS LCCS107. We also measured the transient decay curves of these LC mixtures and obtained the temperature-dependent visco-elastic coefficient  $\gamma_1/K_{11}$ , as the dots presented in Figure 2. The solid lines represent fittings with following relation [27]:

$$\frac{\gamma_1}{K_{11}} = A \frac{\exp(E_a/k_B T)}{(1 - T/T_c)^\beta}. \quad (3)$$

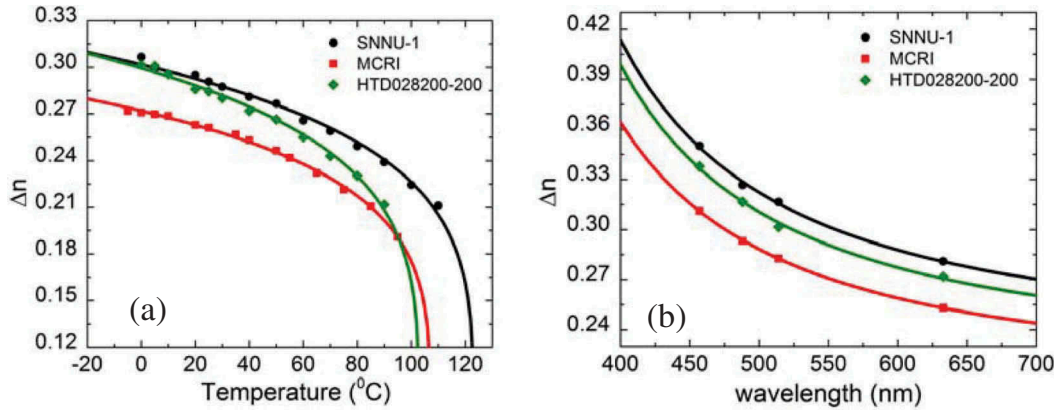
In Equation (3),  $A$ ,  $E_a$  and  $k_B$  stand for the proportionality constant, Boltzmann constant and activation energy, respectively. The fitting parameters used in Figures 1 and 2 are summarised in Table S1.

#### 3.3 Dielectric anisotropy

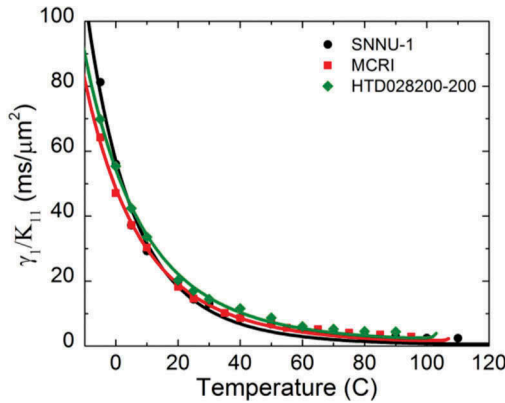
The dielectric constants were measured with a multi-frequency LCR meter HP-4274 and results are listed in Table 2. Compared with SNUU-1, MCRI has a larger  $\Delta\epsilon$ , higher  $\gamma_1$  and lower  $\Delta n$ . The larger  $\Delta\epsilon$  helps to lower the operation voltage, but the multiple polar groups in component #8 dramatically increase  $\gamma_1$  and decrease  $\Delta n$  [28], which would increase the response time. Herein, there is a trade-off between low voltage and fast response time.

#### 3.4 Overall performance

Keeping a  $2\pi$  phase change at low operation voltage ( $V_{2\pi} = 5\text{V}$ ), we used the physical parameters of three LC mixtures to simulate the response time in a



**Figure 1.** (Colour online) (a) Temperature-dependent birefringence at  $\lambda = 633$  nm. (b) Birefringence dispersion at  $40^\circ\text{C}$ . Dots are measured data, and the lines in (a) and (b) are fitting curves with Equations (1) and (2), respectively.



**Figure 2.** (Colour online) Temperature-dependent visco-elastic coefficient at  $\lambda = 633$  nm. Dots are measured data and lines are fitting curves with Equation (3).

reflective cell by a commercial LCD software DIMOS 2.0. The simulated response time (rise + decay) of SNNU-1, MCRI and HTD028200-200 is 4.14, 3.14 and 3.23 ms, respectively. As expected, MCRI with a high birefringence, moderate rotational viscosity and dielectric anisotropy ( $\Delta\epsilon \sim 6.65$ ) exhibits the fastest response time among the three mixtures studied. Along with its high resistivity and wide nematic range, MCRI satisfies the requirements of 240-Hz phase-only LCoS for AR displays. In the following sections, our evaluation will be focused on MCRI.

## 4. Device performances

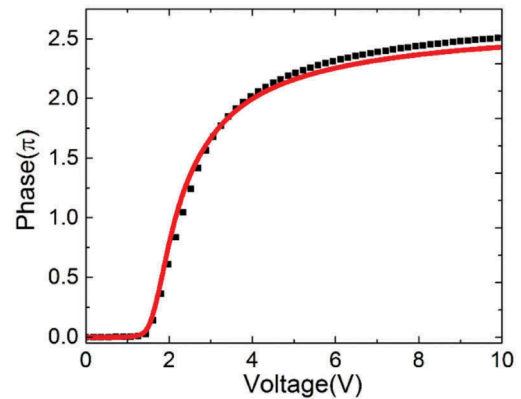
### 4.1 Voltage-dependent phase change (V $\Phi$ ) curve

To simulate the electro-optic performance of MCRI in a real LCoS device, we injected our LC mixture MCRI into a transmissive homogeneous cell with cell gap  $d \approx 3.43$   $\mu\text{m}$ . Then, we measured its voltage-dependent transmittance

(VT) curve and converted the measured VT curve to voltage-dependent phase (V $\Phi$ ) curve. The phase change of this transmissive cell is equivalent to that of a reflective cell with  $d \approx 1.715$   $\mu\text{m}$ , because of the doubled optical path. Figure 3 compares the V $\Phi$  curves converted from the measured VT curve (dots) with the simulated VT curve (red line). Results indicate that the simulated curve fits reasonably well with the experimental data. Therefore, the simulated V $\Phi$  curves can be used for further analysis.

### 4.2 Response time

As shown in Figure 3, we obtained  $\sim 2.21\pi$  phase change at 5V with a 3.43- $\mu\text{m}$  transmissive cell. These values indicate a  $2\pi$  phase change can be obtained at 5V with a 1.55- $\mu\text{m}$  reflective cell. Because the response time ( $\tau$ ) is proportional to  $d^2$  [29], the response time of the 1.55- $\mu\text{m}$  reflective cell should be 4.9 $\times$  faster than that of the 3.43- $\mu\text{m}$  transmissive cell. To validate the conversion, we compared the simu-



**Figure 3.** (Colour online) A V $\Phi$  curve of MCRI. Dots are measured data from a transmissive homogeneous cell with  $d = 3.43$   $\mu\text{m}$ ; the line is a simulated curve in a reflective homogeneous cell with  $d = 1.715$   $\mu\text{m}$ .

**Table 3.** Extrapolated PTP response time of MCRI of a 1.55- $\mu\text{m}$  reflective LCoS panel based on the measured data from a 3.43- $\mu\text{m}$  transmissive cell.

Decay time (ms)	Rise time (ms)								
	1	2	3	4	5	6	7	8	9
<b>1</b>	*	15.43	9.27	5.96	4.42	3.28	2.27	1.31	0.63
<b>2</b>	2.48	*	6.42	3.78	3.55	2.69	1.89	1.05	0.54
<b>3</b>	2.38	7.75	*	3	3.16	2.4	1.69	0.97	0.49
<b>4</b>	2.38	6.73	4.68	*	2.86	2.2	1.54	0.89	0.45
<b>5</b>	2.38	6.18	4.57	3.28	*	2.01	1.36	0.84	0.42
<b>6</b>	2.35	5.62	4.04	3.13	2.41	*	1.33	0.81	0.41
<b>7</b>	2.34	5.17	3.7	2.93	2.35	1.79	*	0.79	0.4
<b>8</b>	2.34	4.85	3.17	2.83	2.26	1.8	1.1	*	0.39
<b>9</b>	2.32	4.56	3.37	2.72	2.21	1.75	1.05	0.76	*

Note: \* no data.

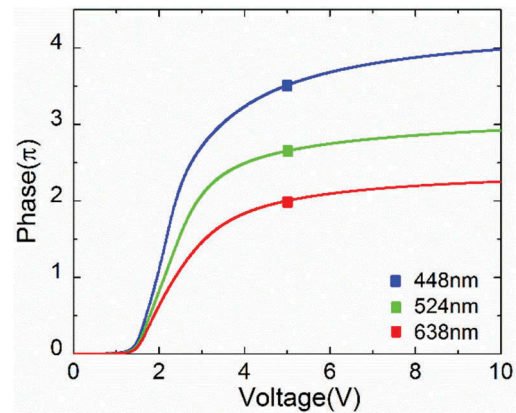
lated response time ([rise, decay] = [0.60 ms, 2.54 ms]) of the 1.55- $\mu\text{m}$  cell with the experimentally extrapolated response time ([rise, decay] = [0.63 ms, 2.32 ms]). The difference is only 6.4%.

In an AR device, each pixel of the LCoS panel should be able to generate any phase level between 0 and  $2\pi$ . To evaluate the grayscale phase response, we divided the phase change into nine levels for further evaluation. Table S2 lists the representative phase levels and the corresponding operation voltages. By measuring the response time between every two phase levels, we can obtain a phase-to-phase (PTP) response time chart as shown in Table 3. The extrapolated average PTP response time of a 1.55- $\mu\text{m}$  reflective LCoS panel is 2.87 ms. That means, the LCoS employing our MCRI mixture can achieve 240 Hz for field sequential colour operation.

Fast response time is indeed achieved under our thin cell strategy. However, manufacturing yield decreases as the cell gap gets thinner. The 1.55- $\mu\text{m}$  cell gap is still manageable for LCoS panels. Other important parameters affecting the LCoS performance are fringing field effect and diffraction effect, especially when the pixel size is small [30]. Fringing field effect, which depends on the LC alignment, e.g. vertical alignment, twisted alignment and homogeneous alignment, have been investigated extensively [31]. A thinner cell gap is helpful to suppress the fringing field effect [30,31].

### 4.3 A full-colour phase-only SLM device

MCRI can also be used in a full-colour phase-only SLM device. In the Microsoft's LCoS-based AR prototypes [4], the wavelengths of the three employed laser diodes are 448, 524 and 638 nm. Therefore, in our simulation, we also chose the same wavelengths. From Figure 1(b) and Equation (2), the  $\Delta n$  at 40°C and  $\lambda = [448 \text{ nm}, 524 \text{ nm}, 638 \text{ nm}]$  is [0.3171, 0.2790, 0.2522]. The cell gap was set at 1.52  $\mu\text{m}$  to ensure  $V_{2\pi} \leq 5\text{V}$  works for the RGB colours. Figure 4 shows the simulated V $\Phi$

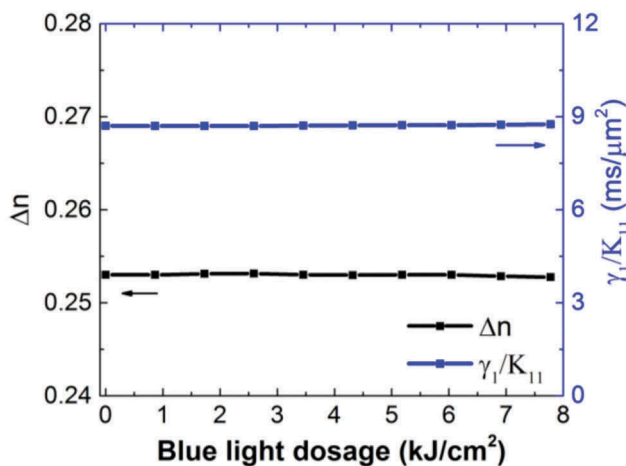


**Figure 4.** (Colour online) Simulated V $\Phi$  curves of MCRI for the specified RGB colours at 40°C in a reflective homogenous cell with  $d = 1.52 \mu\text{m}$ . Lines are V $\Phi$  curves; dots represent the upper limit of the phase change range with 5 V.

curves of MCRI for the RGB wavelengths. For red light with the longest  $\lambda$  and the lowest  $\Delta n$ , its  $V_{2\pi}$  is controlled at 5 V. For the other two colours, more than  $2\pi$  phase change can be obtained at 5 V.

### 4.4 Photostability of MCRI under blue light

For a full-colour phase-only SLM device, red ( $\lambda = 638 \text{ nm}$ ), green ( $\lambda = 524 \text{ nm}$ ) and blue ( $\lambda = 448 \text{ nm}$ ) are the three primary colours. The low-energy red and green photons are much less harmful than the high-energy blue photons. Thus, the photostability of a LC mixture in practical use is determined by the blue light. Taking a 10,000-nits high-brightness backlight unit, for example, the blue light intensity on LCoS panel is about  $10 \text{ mW/cm}^2$ . After 200 working hours, the accumulated dose per unit surface area is  $7.2 \text{ kJ/cm}^2$ . To evaluate the photostability, we injected MCRI into a 5.0- $\mu\text{m}$ -thick homogeneous cell and illuminated it at 40°C by a Helium-Cadmium laser ( $\lambda = 445 \text{ nm}$ ). We monitored and recorded the birefringence ( $\Delta n$ ) and visco-elastic coefficient ( $\gamma_1/K_{11}$ ) of MCRI after blue light exposure. As shown in Figure 5, no obvious sign of



**Figure 5.** (Colour online) Measured photo-stability of MCRI exposed at  $\lambda = 446$  nm and  $40^\circ\text{C}$ . Probing laser beam:  $\lambda = 633$  nm. Measurement temperature:  $40^\circ\text{C}$ . Black dots denote birefringence and blue dots denote visco-elastic constant.

degradation of MCRI is observed after up to  $\sim 8$  kJ/cm<sup>2</sup> of laser irradiation.

## 5. Conclusions

We have developed a new LC mixture (MCRI) for phase-only LCoS based AR displays. MCRI exhibits following physical properties:  $\Delta n = 0.253$ ,  $\Delta\epsilon = 6.65$ ,  $\gamma_1/K_{11} = 8.7$  ms/ $\mu\text{m}^2$  at  $\lambda = 633$  nm and  $T = 40^\circ\text{C}$ . When employing MCRI in a phase-only LCoS for AR displays, the average PTP response time is 2.87 ms, which enables 240 Hz frame rate for field sequential colour operation, while keeping a  $2\pi$  phase change, 5V operation voltage and high resistivity. Potential application of MCRI for the emerging AR displays is foreseeable.

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## Disclosure statement

No potential conflict of interest was reported by the authors.

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