

# Cross talk between bistable elements on an InSb étalon

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Cross talk due to transverse carrier diffusion between identical bistable elements on an InSb étalon at 80 K is studied both theoretically and experimentally. Measurements of cross talk between two such elements show that typically, for a practical system, a critical separation of a few diffusion lengths between beam centers is necessary for independent operation. When the difference between holding and switching powers approaches zero, the results show that the critical distance diverges. Delays as great as 4  $\mu\text{sec}$  have been observed when one element is switched and its neighbor is induced to switch through the cross-talk mechanism. These delays can be partially attributed to critical slowing down, and, in principle, they diverge as the interelement distance is increased toward the critical separation. A theoretical model based on the diffusion equation for the single-pass nonlinear phase shift shows how the critical separation depends on physical parameters and the number of elements forming an array. We found that the relevant interaction is essentially limited to nearest neighbors. When the theory is applied to two bistable elements, good agreement is obtained with the experiments in both the steady and the dynamic states.

## 1. INTRODUCTION

The advent of logic elements based on optical bistability has advanced the possibility of all-optical computing systems. The demonstration of a three-element loop circuit<sup>1</sup> has established the basic format for the serial processing of optically encoded data. A fundamental limit to the achievable serial data rate is the switching speed of the individual bistable elements. However, higher data rates may be developed by using parallel processing. This processing would take the form of an optical array in which all the elements would be involved in the simultaneous but independent handling of information. This method raises a question about packing densities since the minimum separation of elements will in practice be limited by the extent of the transverse coupling between them. This coupling, or cross talk, is not necessarily confined to adjacent elements, but it can be a long-range effect, as in thermal nonlinearities in interference filters<sup>2,3</sup>—with severe consequences on interelement separation necessary for channel isolation.

The object of this paper is to address some of these questions. We report measurements of, and a theoretical model on, transverse-diffusive coupling between two bistable elements on an InSb étalon. The dependence of critical distance ( $d_{\text{crit}}$ ) on the holding power is investigated. ( $d_{\text{crit}}$  is defined<sup>2</sup> as the smallest separation by which an element can sustain itself in the OFF state while the other element is in the ON state.) In addition, we investigate the temporal dependence of the switching process through controlled cross talk by choosing the separation.

The diffusion of photoexcited carriers in InSb has been studied<sup>4</sup> by the angular dependence of degenerate four-wave mixing. The results indicated that the carrier-diffusion length  $l_D$  is  $\sim 60 \mu\text{m}$  in one recombination time. The theoretical model presented here is based on carrier diffusion as the sole transverse coupling mechanism. This is a short-

range effect when compared with thermal diffusion; hence spacing of only a few diffusion lengths is necessary for independent operation of adjacent elements. Furthermore, the theory predicts that for any number of elements forming a two-dimensional array only nearest neighbors influence  $d_{\text{crit}}$ . The critical separation diverges as the holding power approaches the switch point.

In this paper we present a systematic study of the dynamics of cross talk between adjacent bistable channels in an InSb étalon and develop a theory to analyze the geometric aspects and the time dependence of the effects. The implications for all-optical data processing are also considered.

## 2. EXPERIMENT

The experimental layout is shown in Fig. 1. Two beams, A and B, incident upon the étalon of InSb ( $n \approx 10^{14} \text{cm}^{-3}$ ) were produced from the same cw CO laser operating at a frequency of  $\bar{\nu} = 1819 \text{cm}^{-1}$ . Each beam could be independently controlled in incident power and position on the 280- $\mu\text{m}$ -thick étalon held at 80 K in a liquid-nitrogen reservoir cryostat. The beams were linearly polarized at 90° with respect to each other, which allowed discrimination of the two output beams and minimized any optical interference effects.

The procedure to establish  $d_{\text{crit}}$  involved setting up two identical, adjacent bistable channels, A and B, in the étalon. This task was achieved by adjusting beam A with lens  $L_3$  to give optimum beam radius<sup>5</sup> and minimum switching power. Beam B was then adjusted independently, using lens  $L_2$ , so that with beam A blocked, channel B gave identical switching characteristics. An area of  $100 \mu\text{m} \times 1500 \mu\text{m}$  was found on the étalon, over which the switching power was constant to  $\pm 2\%$ , and the cross-talk experiment was confined to this region.

The incident plane of the étalon was imaged into a thermal camera by using lens  $L_4$ , and the channel spacing was

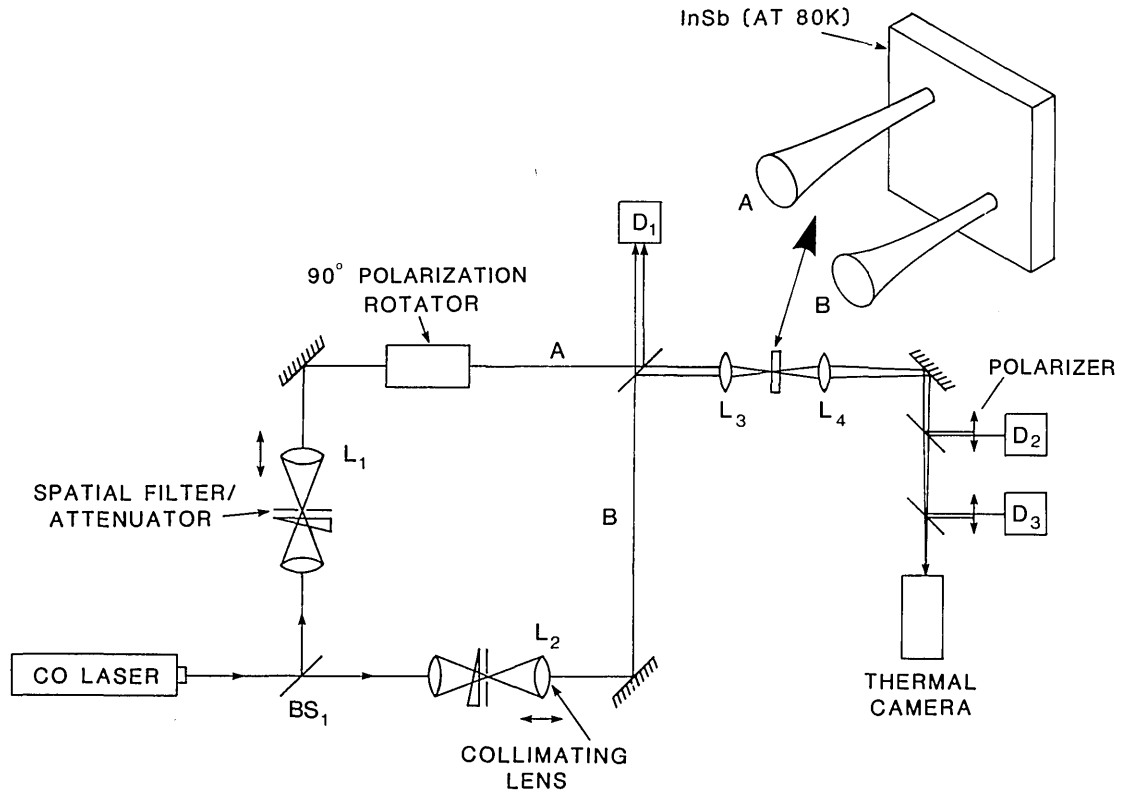


Fig. 1. Schematic of experimental setup: L's, lenses; BS<sub>1</sub>, beam splitter. Both inputs were detected by detector D<sub>1</sub>; individual outputs were detected by detectors D<sub>2</sub> and D<sub>3</sub>.

measured on a monitor screen. The imaging system was calibrated with a precision pinhole of known diameter. In a typical experimental run, beams A and B were set at a chosen separation with identical holding beam powers with the standoff from switching,  $\Delta P$ , determined by

$$\Delta P = (1 - P_{\text{hold}}/P_s)100,$$

where  $P_{\text{hold}}$  is the holding power and  $P_s$  is the single-element switch power. When beam A was switched to the ON state and after a certain time delay, beam B would spontaneously

switch on if there were sufficient transfer of carriers between the channels. Both the channel spacing and the standoff from switching could be varied, and, for a particular setting of  $\Delta P$ , the channel spacing could be increased until transfer of switching ceased. This experimental determination of  $d_{\text{crit}}$  is summarized in Fig. 2. The time delay involved in the transfer of switching is illustrated in Fig. 3(a), and the composite results are summarized in Fig. 3(c), where switch delay times are plotted as a function of  $\Delta P$  for three values of interelement spacing. For small values of  $\Delta P$  (<2%), the

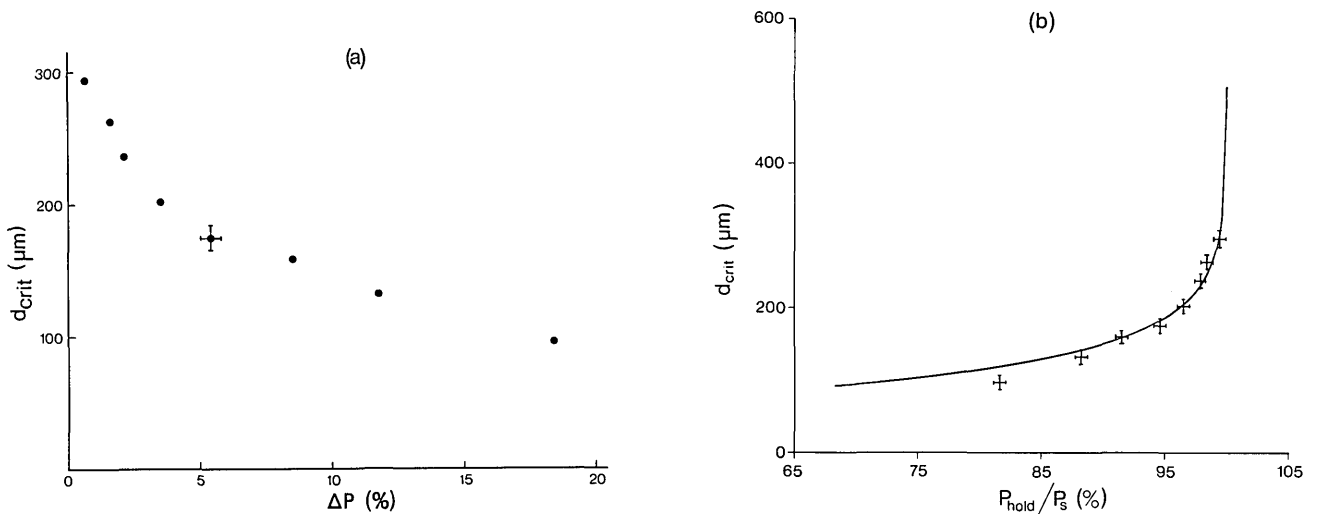


Fig. 2. (a) Experimental determination of the critical separation  $d_{\text{crit}}$  as a function of the stand-off power  $\Delta P$ . (b) Comparison between theory and experiment for critical distance as a function of  $P_{\text{hold}}/P_s$  (%). The solid line corresponds to the solution of Eq. (22) for  $\Phi_0 = 0.45$  and a finesse  $f = 3.5$ . Experimental points are those of (a).

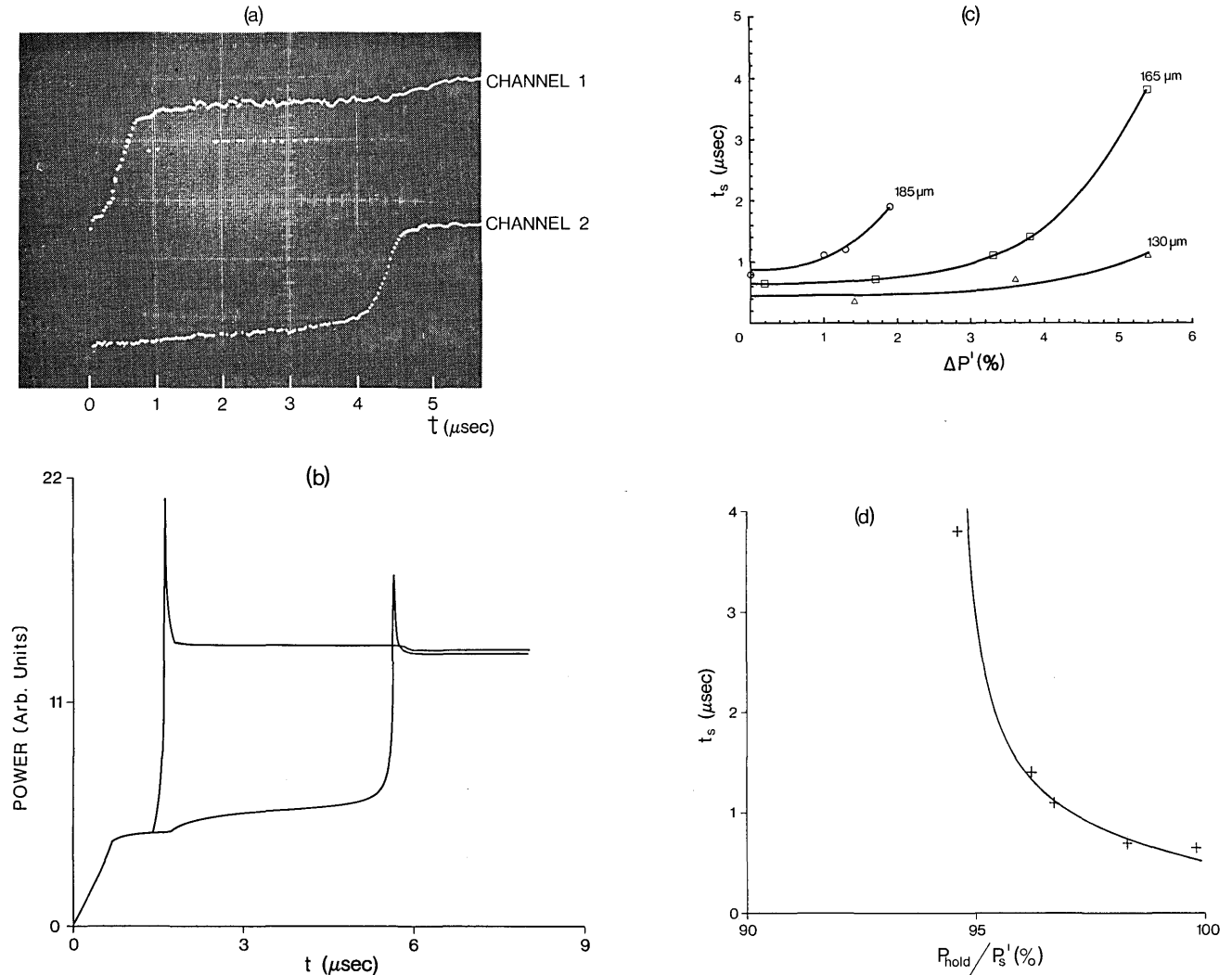


Fig. 3. (a) Oscilloscope trace of the time evolution of the transmitted powers showing the delay between the switching of channel 1 (E1) and channel 2 (E2) for  $d = 165 \mu\text{m}$  and  $\Delta P' \equiv (1 - P_{\text{hold}}/P_s')100 = 5.2\%$ , where  $P_s' \propto I_s'$  (see Section 3). Here  $d_{\text{crit}} \approx 180 \mu\text{m}$ . (b) Numerical simulation of (a) for the transmitted powers by solving Eq. (14). Note that the sharp overshooting is the result of calculating at beam centers: parameters,  $f = 3.5$ ,  $\Phi_0 = 0$ . (c) Experimental plot of the time delay versus  $\Delta P$  for various separations. (d) Switching times as in (c) but in terms of  $P_{\text{hold}}/P_s'$  (%). Note that  $P_s'$  changes with separation. Solid line corresponds to theory for  $\Phi_0 = 1.8$  and  $w = 0.5l_D$ .

time delay is simply the transit time for carriers to diffuse from element A to B, but at larger values of  $\Delta P$ , where the transfer of switching becomes more marginal, the switching process is subject to critical slowing-down effects, and microsecond delays are observed. The implications of these results are discussed in Section 4.

### 3. THEORY

In this section the theory is developed by starting with an outline of the general equations from which the derivation<sup>6,7</sup> of the diffusion equation for the single-pass nonlinear phase shift  $\Phi$  is obtained. By using the appropriate Green function, a system of integral equations for  $\Phi$  at each beam center, in both the time-dependent and steady states, is derived. Then critical separations and their dependence on detuning, finesse, and spot radius are calculated.

Consider a nonlinear medium in a Fabry-Perot resonator of mirror reflectivities  $R_F$  (front) and  $R_B$  (back) where light propagates in the  $z$  direction. We assume that the local

refractive index is given by  $n = n_0 + n_2 I_c$ , where  $I_c$  is the internal intensity, and that the cavity round-trip time is  $\tau_r \ll \tau$  (recombination time). Then, after adiabatic elimination of the field variables and in the limit of strong diffusion, we can write

$$\partial F(\mathbf{r}, z, t)/\partial z = [-(\alpha L/2) + iN(\mathbf{r}, z, t) + i(\mathcal{F}/2)\nabla_T^2]F(\mathbf{r}, z, t), \quad (1)$$

$$-\partial B(\mathbf{r}, z, t)/\partial z = [-(\alpha L/2) + iN(\mathbf{r}, z, t) + i(\mathcal{F}/2)\nabla_T^2]B(\mathbf{r}, z, t), \quad (2)$$

$$l_T^2 \nabla_T^2 N(\mathbf{r}, z, t) + l_L^2 \partial^2 N(\mathbf{r}, z, t)/\partial z^2 - \tau \partial N(\mathbf{r}, z, t)/\partial t - N(\mathbf{r}, z, t) = -4\mathcal{F} \text{sgn}(n_2)(|F(\mathbf{r}, z, t)|^2 + |B(\mathbf{r}, z, t)|^2), \quad (3)$$

where

$$\begin{bmatrix} F \\ B \end{bmatrix} = (n_0 c / 16 P_c)^{1/2} \begin{bmatrix} E_f \\ E_b \end{bmatrix}$$

are the scaled forward and backward electric field envelopes,  $c$  is the speed of light,  $P_c = \lambda^2/2\pi n_0|n_2|$  is the critical power for self-focusing,  $\mathcal{F} = \lambda L/2\pi n_0 \omega^2$  is the Fresnel number,  $L$  is the cavity length,  $w$  is the spot radius,  $\nabla_T^2 = \partial^2/\partial x^2 + \partial^2/\partial y^2$  is the transverse Laplacian scaled to  $w^2$ ,  $N$  is the excitation density,  $z$  is scaled to  $L$ ,  $l_T \equiv l_D/w$ ,  $l_L \equiv l_D/L$ , and  $l_D = (D\tau)^{1/2}$ , and  $D$  is the diffusivity.

Equations (1)–(3) can be derived from the Maxwell–Bloch equations in the limit of high dispersion<sup>8</sup> where the excitation density is a scaled population inversion. Unless  $l_D \gg \lambda$  we should also include population-grating terms (standing-wave effects), which double the phase shift imposed on the counterpropagating fields by each other (nonlinear nonreciprocity). In this section an InSb étalon in which  $N$  is the photogenerated-carrier concentration is considered.

The boundary conditions of this problem are

$$F(\mathbf{r}, 0, t) = (1 - R_F)^{1/2} F_{in}(\mathbf{r}, t) + R_F^{1/2} B(\mathbf{r}, 0, t) \exp(-2i\Phi_0), \quad (4)$$

$$B(\mathbf{r}, 1, t) = R_B^{1/2} F(\mathbf{r}, 1), \quad (5)$$

$$N(\mathbf{r}, z, t) \rightarrow 0 \quad \text{as } |\mathbf{r}| \rightarrow \infty, \quad (6)$$

$$(l_T^2/\tau)\partial N(\mathbf{r}, p, t)/\partial z = N(\mathbf{r}, p, t)S \quad (p = 0, 1), \quad (7)$$

where  $\Phi_0$  is the linear cavity detuning and  $S$  is the surface-recombination velocity. In the present experimental conditions we can neglect diffraction in Eqs. (1) and (2) since for  $L = 280 \mu\text{m}$  and  $\lambda = 5.5 \mu\text{m}$  we get an effective diffraction area  $\lambda L = 1540 \mu\text{m}^2$  smaller than  $l_D^2$  ( $\sim 3600 \mu\text{m}^2$ ). Then, defining the single-pass nonlinear phase shift

$$\Phi(\mathbf{r}, t) \equiv \int_0^1 dz N(\mathbf{r}, z, t), \quad (8)$$

and after integrating over  $z$ , neglecting surface effects ( $S = 0$ ), and using expressions (4)–(8) in Eqs. (1)–(3), we get

$$l_T^2 \nabla_T^2 \Phi(\mathbf{r}, t) - \tau \partial \Phi(\mathbf{r}, t) / \partial t - \Phi(\mathbf{r}, t) = -I_{in}(\mathbf{r}, t) A[\Phi(\mathbf{r}, t)], \quad (9)$$

with

$$A[\Phi(\mathbf{r}, t)] = 1/|1 + f \sin^2[\Phi(\mathbf{r}, t) - \Phi_0]| \quad (\text{Airy function})$$

$$I_{in}(\mathbf{r}, t) = -4\mathcal{F}[1 - \exp(-\alpha L)][(1 - R_F)(1 + R_B)]$$

$$\times |F_{in}|^2/\alpha L(1 - R_\alpha)^2,$$

$$R_\alpha = (R_F R_B)^{1/2} \exp(-\alpha L),$$

$$f = 4R_\alpha/(1 - R_\alpha)^2.$$

Equation (9) is the starting point, and the concentration will be obtained by solving for a solution at the beam center, where the switching is most relevant. To deal with arrays it is convenient to transform Eq. (9) into an integral equation by using the corresponding Green function (see Appendix A) given by

$$G(\mathbf{r} - \mathbf{r}', t - t') = \exp[-(\mathbf{r} - \mathbf{r}')^2/4(t - t')] \times \{\exp[-(t - t')]/4\pi(t - t')\}, \quad (10)$$

in which the space variables are scaled to  $l_D$  and  $t$  is scaled to  $\tau$  as it follows naturally from Eq. (9); this scaling is kept throughout. The formal solution then reads as

$$\Phi(\mathbf{r}, t) = \Phi(\mathbf{r}, -\infty) + \int_{-\infty}^t dt' \int_{\mathbf{r}'} d^2\mathbf{r}' G(\mathbf{r} - \mathbf{r}', t - t') \times I_{in}(\mathbf{r}', t') A[\Phi(\mathbf{r}', t')]. \quad (11)$$

For  $N$  beams,

$$I_{in}(\mathbf{r}, t) = \sum_{j=1}^N I_j(t) \exp[-(\mathbf{r} - \mathbf{r}_j)^2/W^2], \quad (12)$$

$$W \equiv w/l_D,$$

where  $\mathbf{r}_j$  is the position of the center of the  $j$ th beam. On substitution of Eq. (12) into Eq. (11) we can ignore the variation<sup>9</sup> of  $\Phi(\mathbf{r}, t)$  over the spatial integration if  $W < 1$  or  $W \rightarrow \infty$  (plane-wave approximation). If we take  $W < 1$ —which in fact corresponds to the experimental situation—we can replace  $\Phi(\mathbf{r}, t)$  by  $\Phi(\mathbf{r}_j, t) \equiv \Phi_j(t)$  in Eq. (11). Using Eqs. (10) and (12) in Eq. (11) and assuming that  $\Phi(\mathbf{r}, -\infty) = 0$ , we obtain

$$\Phi_i(t) = \int_{-\infty}^t dt' \int_{\mathbf{r}'} d^2\mathbf{r}' G(\mathbf{r}_i - \mathbf{r}', t - t') \times \sum_{j=1}^N I_j(t') \exp[-(\mathbf{r}' - \mathbf{r}_j)^2/W^2] A_j(t') \quad (i = 1, 2, \dots, N), \quad (13)$$

where  $A_j(t') \equiv A[\Phi_j(t')]$ . Integration over space variables leads to the following system of integral equations:

$$\Phi_i(t) = \int_{-\infty}^t dt' \sum_{j=1}^N A_j(t') I_j(t') W^2 \times \{\exp[-d_{ij}^2/(W^2 + 4(t - t'))] - (t - t')/[W^2 + 4(t - t')]\} \quad (i = 1, 2, \dots, N), \quad (14)$$

where  $d_{ij}^2 \equiv (\mathbf{r}_i - \mathbf{r}_j)^2$ .

In the steady state each  $\Phi_i$  is constant in time; thus from Eq. (14)

$$\Phi_i = \sum_{j=1}^N A_j I_j M(d_{ij}) \quad i = 1, 2, \dots, N, \quad (15)$$

with  $M(d_{ij})$  being the coupling coefficient:

$$M(d_{ij}) \equiv (W^2/4) \exp(W^2/4) \int_{W^2/4}^{\infty} du \exp(-d_{ij}^2/u - u)/u. \quad (16)$$

If  $N = 1$ , then  $d_{ij} \equiv 0$ , and we can explore the dependence of the switching power on the spot size

$$\Phi = A(\Phi) P \exp(W^2/4) E_i(W^2/4),$$

where  $P \equiv IW^2/4$  is the scaled power and  $E_i$  is the exponential integral; then the switching power is such that

$$P_s \propto \exp(-W^2/4)/E_i(W^2/4). \quad (17)$$

Because  $E_i \rightarrow \infty$  as  $W \rightarrow 0$ , the switching power decreases with spot size, as shown in Fig. 4. These results agree with those previously found both theoretically<sup>7</sup> and experimentally.<sup>5</sup> In the opposite limit, namely,  $W \rightarrow \infty$ , from expression (17),  $P_s \propto W^2$  and thus the plane-wave limit is regained.

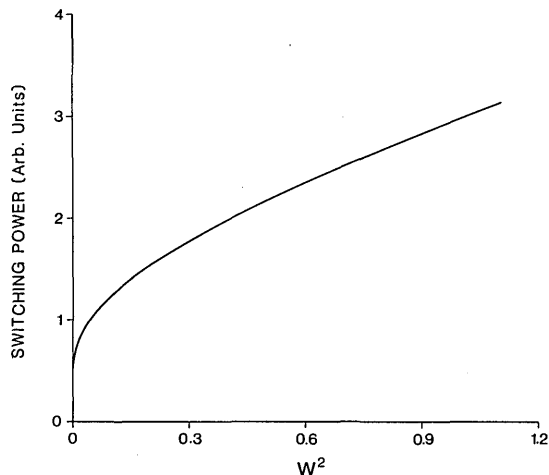


Fig. 4. Plot of switching power as a function of  $W^2$  ( $=W^2/l_D$ ) according to expression (17).

To work out the critical separation between elements we take two elements, E1 and E2, both with identical individual bistable characteristics and holding intensities  $I_{\text{hold}}$ . Then we assume that both elements are initially in the OFF state. Then E1 is suddenly switched on, and therefore the local-carrier concentration increases. As a result, diffusion from E1 into E2 occurs, which effectively changes the detuning of E2 and, with it, the bistable characteristic. Consequently the switching intensity  $I_s$  of E2 changes to a new<sup>3</sup> value  $I_s' < I_s$  such that if  $d_{12} > d_{\text{crit}}$ ,  $I_s' > I_{\text{hold}}$ , and E2 stays off; if  $d_{12} < d_{\text{crit}}$  it follows that  $I_s' < I_{\text{hold}}$ , and E2 switches on. However, if  $d_{12} = d_{\text{crit}}$ , then  $I_s' = I_{\text{hold}}$ , and this defines  $d_{\text{crit}}$  from the relation

$$\partial I_2 / \partial \Phi_2 |_{I_2 = I_{\text{hold}}} = 0, \quad (18)$$

as explained below. Equation (18) is widely used to work out threshold parameters of bistable loops.

We can extend the above idea to a two-dimensional array by forming a square lattice for which we try to find the smallest lattice constant  $d$  such that the most unfavorably placed element EM—the one approximately in the middle—can sustain itself in the OFF state while all the others are on. Then, if EM is the  $m$ th element, the equivalent condition to Eq. (18) is

$$\partial I_m / \partial \Phi_m |_{I_m = I_{\text{hold}}} = 0, \quad (19)$$

which can be worked out by reexpressing Eq. (15) as

$$\Phi_m = A(\Phi_m)I_m M(0) + \sum_{j=1}^N A(\Phi_j)I_j M(d_{jm})(1 - \delta_{jm}), \quad (20)$$

where  $\delta_{jm}$  is Kronecker's delta. Similar equations should in principle be added on for the remaining  $N - 1$  phases. However, one can approximate  $\Phi_j$  to a value  $\Phi_{\text{up}}$  for every  $j \neq m$  since the smaller slope of the upper branch prevents appreciable changes of the  $\Phi_j$ 's owing to changes in  $\Phi_m$ . This fact was confirmed by the numerical simulations using Eq. (15); a similar effect occurs with the temperature in interference filters.<sup>2</sup> With this assumption we can apply Eq. (19) to Eq. (20) to obtain

$$I_{\text{hold}} M(0) f \sin 2(\Phi_c - \Phi_0) A^2(\Phi_c) + 1 = 0, \quad (21)$$

where  $\Phi_c$  is the value of  $\Phi_m$  at the switch-up point. Once we have solved for  $\Phi_c$  in Eq. (21), substitution into Eq. (20) yields

$$\Phi_c = A(\Phi_c)I_{\text{hold}}M(0) + A(\Phi_{\text{up}})I_{\text{hold}} \sum_{j=1}^N (1 - \delta_{jm})M(d_{\text{crit}}\rho_{jm}), \quad (22)$$

where  $\rho_{jm} \equiv d_{jm}/d_{\text{crit}}$ ;  $\rho_{jm}$  is a factor that depends on the relative position of the elements; for example, for two beams  $\rho_{12} = 1$ . Using Eq. (16) in Eq. (22), we can find the critical lattice constant  $d_{\text{crit}}$ . Figure 2(b) shows very good agreement between the prediction of Eq. (22) for two elements and the experiments when the corresponding parameters are used. The numerical solution of Eq. (14) agrees with the observed time delays, as shown in Fig. 3.

#### 4. DISCUSSION

The present study of bistable cross talk differs from earlier work<sup>10,11</sup> on the transphaser type in which single-valued transfer curves with a region of large differential gain were used. Large element separations ( $\sim 5 l_D$ ) were required for near-independent operation, as any photogenerated carriers induced by, for example, E1, would continually diffuse to E2. However, between bistable elements there exists a logic cross talk in that the device will either be induced to switch or not with effectively no intermediate steady state. Moreover, as explained in Section 3, the diffused carriers from E1 have to produce a significant detuning in E2 to reduce the threshold below the holding power in order for it to switch. This result depends on the initial  $\Delta P$ . We can then expect smaller separations than those of transphaser arrays. For example, from Fig. 2(a), if  $\Delta P = 7\%$ , then  $d_{\text{crit}} \sim 160 \mu\text{m}$ , which would allow a packing density of  $4 \times 10^3 \text{ cm}^{-2}$ .

Time delays  $t_s$  ranging from 1 to 4  $\mu\text{sec}$  were measured. For a fixed  $\Delta P$ ,  $t_s$  increased as  $d$  approached  $d_{\text{crit}}$  from below, and we can expect  $t_s \rightarrow \infty$  as  $d \rightarrow d_{\text{crit}}$  since for  $d > d_{\text{crit}}$ , by definition, there is no switching. The divergence of the time delay is attributed to critical slowing down,<sup>12</sup> which occurs as the threshold power  $P_s'$  (corresponding to  $I_s'$  defined in Section 3) approaches  $P_{\text{hold}}$  from below. In the standard critical slowing-down experiments through stepwise excitation,  $P_{\text{hold}} \rightarrow P_s$ , showing a symmetry with respect to our experiment. This effect was also found in the numerical integration<sup>13</sup> of Eq. (14) for two elements. A comparison between theory and experiment is shown in Fig. 3(d). To integrate Eq. (14) we assumed that both elements were initially in a steady state given by the solution of Eq. (15). Then an addressing pulse switches E1, which in turn switches E2 through cross talk at some time  $t_s$  later that depends on how close  $d$  is to  $d_{\text{crit}}$ . In Fig. 3(d) the observed time delay is plotted for  $d = 165 \mu\text{m}$  as the fraction  $I_{\text{hold}}/I_s$  is changed together with the corresponding predictions of the theory.

The effects of spot size, detuning, and finesse on  $d_{\text{crit}}$  for two elements were studied numerically. In Fig. 5(a) the variation of  $d_{\text{crit}}$  against  $I_{\text{hold}}/I_s$  for various values of  $w/l_D$  is shown. As expected,  $d_{\text{crit}}/w$  increases as  $w$  is decreased since the intensity increases<sup>8</sup> (and with it the carrier-concentration gradient) and therefore relatively more diffusion occurs.

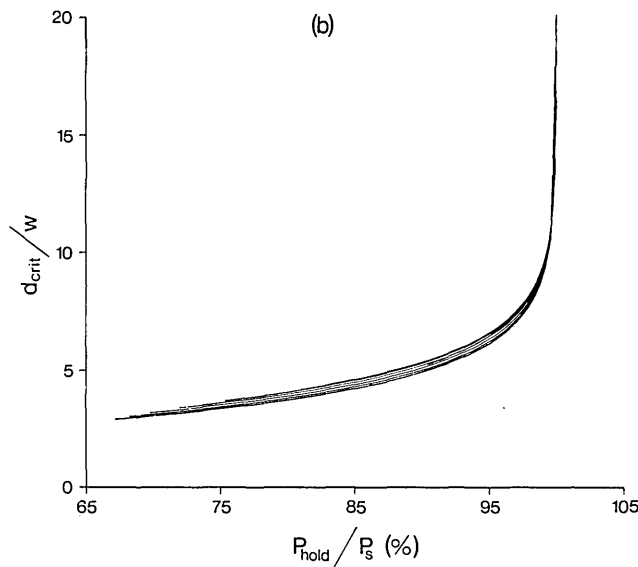
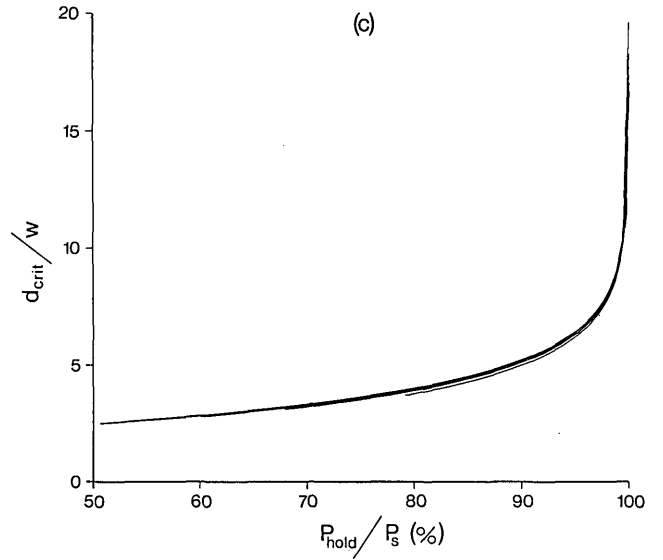
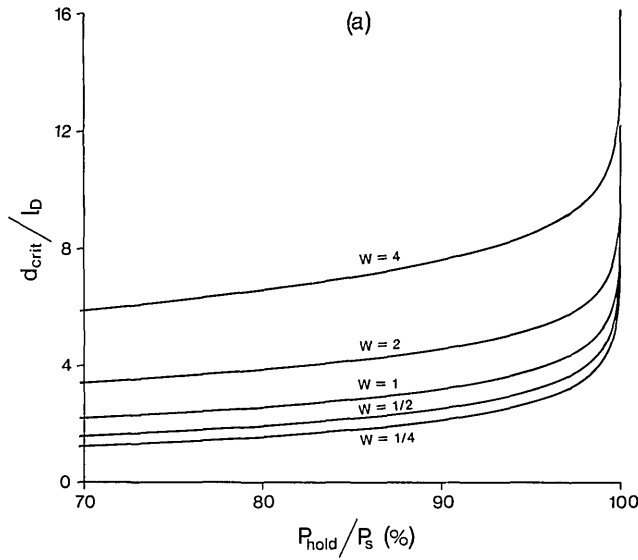


Fig. 5. Plot of critical distance as a function of  $P_{\text{hold}}/P_s$  according to Eq. (22): (a) for  $w/l_D = 0.25, 0.5, 1, 2, 4$ , in the upward direction; note that as  $w$  increases,  $d_{\text{crit}}/w$  decreases for a given holding intensity. Here  $f = 3.5$  and  $\Phi_0 = 0$ . (b) The same plot for  $0 \leq \Phi_0 \leq \pi$ ,  $f = 3.5$ , and  $w/l_D = 0.5$ . (c) The same plot for  $2 \leq f \leq 128$ , and  $w/l_D = 0.5$ , and  $\Phi_0 = 0$ . In all cases the bistable mode of operation was ensured.

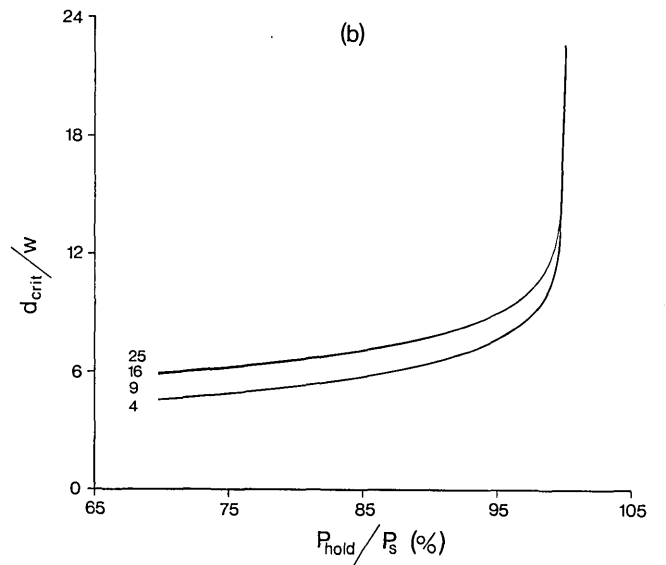
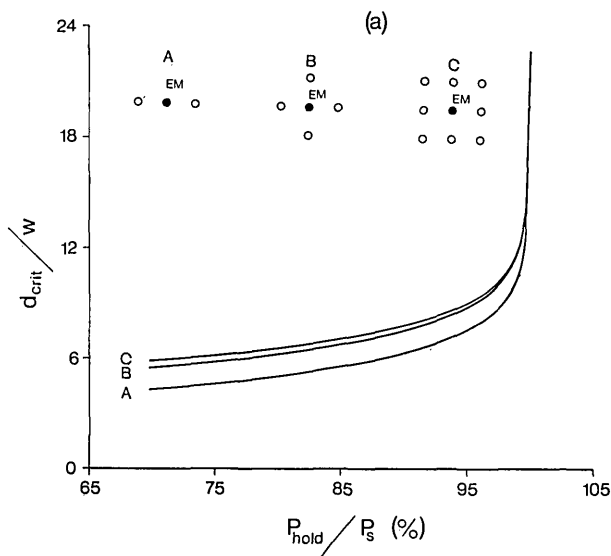


Fig. 6. Effect on the critical lattice constant as an element is surrounded by an increasing number of pixels in the ON state. In all cases  $w = 0.5l_D$ ,  $f = 3.5$ , and  $\Phi_0 = 0$ : (a) letters on curves refer to configurations in the inset; (b) same as (a) but for 4-, 9-, 16-, and 25-element matrices.

Figures 5(b) and 5(c) show slight variations with detuning and finesse, respectively.

In Fig. 6(a) a simulation is shown of the effect of surrounding EM by two (A), four (nearest neighbors) (B), and eight (four nearest neighbors, four next-nearest neighbors) (C) elements on a square lattice. In going from two to four elements the difference is apparent, but when the next-nearest neighbors are added on, the critical lattice constant  $d_{\text{crit}}$  changes negligibly. This observation confirms previous findings<sup>9</sup> through heuristic arguments that, in systems with carrier diffusion as the transverse coupling mechanism, the interaction is limited to nearest neighbors. In Fig. 6(b) these calculations are extended to up to 25 elements with a barely noticeable difference, in sharp contrast to interference filters, which have a long-range coupling through thermal diffusion.

## 5. CONCLUSIONS

In this paper bistable cross talk between elements on an InSb Fabry-Perot étalon was studied. The minimum separation for independent operation increases with the diffusion length, thus limiting the packing density of elements. This latter aspect, however, could be improved further by combinations of the following. First, the element's size can be decreased. However, as the numerical simulations of the present work imply, the carrier profile does not decrease proportionally. Second, it is not mandatory to use pure bulk InSb. If a large number of impurities were introduced they would reduce the carrier lifetime and thus the diffusion length, but the power requirements would be greater. Another possibility would be actual material pixellation by etching one surface of the étalon to give a grid structure.

An important figure of merit in optical computing is the data-processing rate, defined as the product between packing density and switching rate (bits  $\text{sec}^{-1} \text{cm}^{-2}$ ). The present switching rate for dispersive optical bistability in high-purity InSb is  $\sim 10^6 \text{sec}^{-1}$ , which, with a packing density of  $10^3 \text{cm}^{-2}$ , would give a data rate of  $\sim 10^9 \text{bits sec}^{-1} \text{cm}^{-2}$ . Pixellation of the sample and reduction of the element's size may stretch packing densities to up to  $10^5 \text{cm}^{-2}$ , and, with increasing speeds due to impurity doping, data rates of  $10^{13} \text{bits sec}^{-1} \text{cm}^{-2}$  may be possible. The observed optical delays in the microsecond region are required in some applications. Conventional methods of producing them, such as long path lengths, are bulky and often distort the beam. The present experiments suggest a compact technique to produce such delays. Finally, by choosing the appropriate separations, controllable cross talk could be used to perform logic functions in future computer architectures.

## APPENDIX A

To obtain Green's function for this problem a particular solution of

$$-\nabla^2 G(\mathbf{r} - \mathbf{r}', t - t') + \partial G(\mathbf{r} - \mathbf{r}', t - t')/\partial t + G(\mathbf{r} - \mathbf{r}', t - t') = \delta(\mathbf{r} - \mathbf{r}', t - t') \quad (\text{A1})$$

has to be found, where the spatial coordinates lie in the  $x$ - $y$  plane and  $G$  is Green's function with a Fourier transform  $\tilde{G}(\mathbf{k}, \omega)$  such that

$$G(\mathbf{r} - \mathbf{r}', t - t') = \iint_{-\infty}^{\infty} \int d^2\mathbf{k} d\omega \tilde{G}(\mathbf{k}, \omega) \times \exp[i\mathbf{k} \cdot (\mathbf{r} - \mathbf{r}') + i\omega(t - t')]. \quad (\text{A2})$$

Then on substitution of Eq. (A2) into Eq. (A1) and using the Fourier transforms of the delta functions,

$$\tilde{G}(\mathbf{k}, \omega) = -i/(2\pi)^{3/2}[\omega - i(k^2 + 1)]. \quad (\text{A3})$$

By using Eq. (A3) in Eq. (A2), the integral over  $\omega$ ,

$$f(k) = \int_{-\infty}^{\infty} d\omega \exp[i\omega(t - t')]/[\omega - i(k^2 + 1)], \quad (\text{A4})$$

can be solved exactly in the complex plane, yielding

$$f(k) = 2\pi i \exp[-(k^2 + 1)(t - t')],$$

and consequently

$$\begin{aligned} G(\mathbf{r} - \mathbf{r}', t - t') &= \exp[-(t - t') - (\mathbf{r} - \mathbf{r}')^2/4(t - t')] (2\pi)^{-2} \iint_{-\infty}^{\infty} dk_x dk_y \\ &\times \exp\{-[k_x(t - t')^{1/2} - i(x - x')/2(t - t')^{1/2}]^2\} \\ &\times \exp\{-[k_y(t - t')^{1/2} - i(y - y')/2(t - t')^{1/2}]^2\}. \end{aligned}$$

Finally,

$$G(\mathbf{r} - \mathbf{r}', t - t') = \frac{\exp\{-(t - t') - [(\mathbf{r} - \mathbf{r}')^2/4](t - t')\}}{4\pi(t - t')}.$$

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